

# HUMIDITY SENSOR

## BACKGROUND OF THE INVENTION

### 1. Field of the Invention:

The present invention relates to a humidity sensor for measuring the moisture content of an atmosphere by means of change in the electrical resistance of a moisture sensitive layer. The humidity sensor can be used, for example, for measuring the moisture content of air; the moisture content of exhaust gas of an internal combustion engine of, for example, an automobile, ship, or airplane, particularly the moisture content of an atmosphere containing substantially no oxygen and containing a reducing gas; or the moisture content of a highly reducing atmosphere surrounding a fuel electrode or an air electrode of a fuel cell.

### 2. Description of the Related Art:

Commercially available humidity sensors include resistance-variable-type humidity sensors utilizing adsorption and desorption of water molecules; and capacitance-variable-type humidity sensors utilizing a change in capacitance. Such humidity sensors are formed, for example, from a moisture sensitive ceramic material such as  $\text{Al}_2\text{O}_3$ ,  $\text{MgCr}_2\text{O}_4\text{-TiO}_2$ ,  $\text{TiO}_2\text{-V}_2\text{O}_5$ , or  $\text{ZrCr}_2\text{O}_4\text{-LiZrVO}_4$ . Most of the humidity sensors measure moisture content by means of a change in electric resistance.

A typical humidity sensor formed from such a moisture sensitive ceramic material includes an insulating substrate, a lower electrode formed on

the substrate, a moisture sensitive layer provided on the lower electrode, and an upper electrode formed on the moisture sensitive layer. In many cases, the lower and upper electrodes are formed from a porous body of  $\text{RuO}_2$  in order to enhance the strength of adhesion between the insulating substrate and the moisture sensitive layer, and to cause water vapor contained in air to easily pass through the moisture sensitive layer easily.

### 3. Problems Solved by the Invention:

When an electrode formed from  $\text{RuO}_2$  is exposed to a reducing atmosphere in an exhaust pipe of an automobile or in a specific portion of a fuel cell where the oxygen content is very low and temperature changes over a wide range (e.g.,  $-40^\circ\text{C}$  to  $750^\circ\text{C}$ ), the electrode may be impaired with the passage of time. The problem then arises that the humidity sensor cannot detect a change in the resistance of the moisture sensitive material even though the humidity changes.

### SUMMARY OF THE INVENTION

The present invention contemplates solving the aforementioned conventional problems of the prior art. It is therefore an object of the present invention to provide a humidity sensor of very high accuracy, which can maintain stable humidity detection performance over a long period of time even when the sensor is exposed to an atmosphere containing a very small amount of oxygen and a considerable amount of a reducing gas, such as the atmosphere in the exhaust pipe of an automobile.

The present inventors discovered that when lower and upper electrodes of a humidity sensor are formed from a noble metal exhibiting excellent heat resistance and corrosion resistance, such as platinum or gold, and the upper electrode is joined to a moisture sensitive layer and an electric insulating substrate, the moisture sensitive layer and the substrate can satisfactorily adhere to each other. A humidity sensor having this configuration exhibits enhanced durability, and can maintain excellent humidity detection performance over a long period of time. This is the case even when the sensor is exposed to an atmosphere which undergoes a drastic change in temperature and contains a very small amount of oxygen and a considerable amount of a reducing gas, such as the atmosphere in an exhaust pipe of an automobile; or even when the sensor is provided, for example, in a fuel or air feeding line of a fuel cell.

The present invention has been accomplished on the basis of this finding.

In a first embodiment of the invention, the humidity sensor comprises an insulating substrate, and a lower electrode, a moisture sensitive layer and an upper electrode successively formed on the insulating substrate, wherein the lower electrode comprises a noble metal, the upper electrode comprises a noble metal porous body, and the upper electrode is joined to the moisture sensitive layer and a portion of the insulating substrate.

The aforementioned "insulating substrate" may comprise a ceramic material such as  $\text{Al}_2\text{O}_3$  or  $\text{ZrO}_2$ . Of these ceramic materials, alumina, which

exhibits an excellent insulating property and mechanical strength and is advantageous in terms of cost, is widely employed. No particular limitation is imposed on the thickness and dimensions of the insulating substrate, but typically, the substrate is formed into a rectangular plate-like body having a  
5 thickness of 0.3-2.0 mm, and planar dimensions (width and length) of  $3 \times 10$  mm to  $8 \times 50$  mm.

The aforementioned "lower electrode" and "upper electrode" comprise at least one noble metal selected from among Au, Ag, Ru, Rh, Pd, Os, Ir and Pt. The electrodes may be formed from an alloy containing two or more of  
10 these noble metals. For example, a combination of Pt and Rh is useful, since evaporation of Pt at high temperature is suppressed. The lower electrode and the upper electrode are not necessarily formed from the same noble metal, but the electrodes are preferably formed from the same noble metal. This is because the process for forming the electrodes can be simplified and  
15 simultaneous firing of the electrodes can be carried out easily. Of these noble metals, Au or Pt is preferred. Particularly preferably, as described in a second embodiment of the invention, either or both of the electrodes predominantly contains Pt in an amount of 80% or more by weight. Pt does not easily oxidize at high temperature, does not diffuse in the moisture sensitive layer,  
20 and has a sufficiently high melting point. Therefore, when the lower and upper electrodes are formed from Pt, the humidity sensor exhibits further enhanced durability. The electrodes formed from the aforementioned noble metal may contain other components or impurities, so long as such "other

components or impurities" do not greatly affect the properties of the electrodes.

Since the upper electrode is formed of a noble metal porous body, moisture can easily penetrate the upper electrode and reach the moisture sensitive layer. Therefore, absorption and desorption of water molecules smoothly proceed at the moisture sensitive layer. In order to promote absorption and desorption of water molecules at the moisture sensitive layer, moisture preferably reaches the entirety of the surface of the moisture sensitive layer. Therefore, as described in a third embodiment of the invention, preferably, not only the upper electrode but also the lower electrode comprises a porous body. When the moisture penetrability of the upper and lower electrodes is higher than that of the moisture sensitive layer, which is also formed of a porous body, moisture easily reaches the moisture sensitive layer. Thus, in general, in order to facilitate moisture penetration through the electrodes, the pores in the upper and lower electrodes are made larger than those in the moisture sensitive layer. The size of pores in the upper and lower electrodes is preferably 0.5-20  $\mu\text{m}$ , and the size of pores in the moisture sensitive layer is preferably 0.05-0.1  $\mu\text{m}$ . In order to form the upper and lower electrodes exhibiting preferable moisture penetrability and conductivity, particles of ceramic such as alumina or zirconia are preferably incorporated, in an amount of 1-20 wt.%, into the upper and lower electrodes. The ceramic particle content is preferably at least 1 wt.% to effectively improve the moisture permeability of the electrodes. In contrast, the ceramic particle

content is preferably 20 wt.% or less to reliably prevent poor electrode conductivity.

The aforementioned "moisture sensitive layer" may be formed from a variety of moisture sensitive materials. Examples of the moisture sensitive materials include moisture sensitive ceramic materials, such as  $\text{Al}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ - $\text{TiO}_2$ - $\text{SnO}_2$ ,  $\text{MgCr}_2\text{O}_4$ - $\text{TiO}_2$ ,  $\text{TiO}_2$ - $\text{V}_2\text{O}_5$ ,  $\text{ZrCr}_2\text{O}_4$ - $\text{LiZrVO}_4$ ,  $\text{ZnCrO}_4$ ,  $\text{TiO}_2$ - $\text{SnO}_2$ , and NASICON (Na-Super Ionic Conductor). When the moisture sensitive layer is formed from a moisture sensitive material containing a plurality of oxides, the proportions of the oxides are not particularly limited; i.e., the moisture sensitive layer may be formed from a generally used moisture sensitive material.

The humidity sensor as described in the first embodiment of the inventions including the insulating substrate, the lower electrode, the moisture sensitive layer, and the upper electrode, can be used in practice by connecting lead wires to and extending from the upper and lower electrodes, in order to obtain an output from the sensor. However, as described in a fourth embodiment of the invention, preferably, the humidity sensor comprises a heater provided in the insulating substrate. When the humidity sensor is periodically heated by means of the heater, moisture and other impurities that have invaded the moisture sensitive layer can be completely removed. Through this removal, the moisture sensitive layer is always maintained in a clean state, detection accuracy is enhanced, and the sensor maintains excellent detection characteristics over a long period of time. Even when the humidity

is very high, dew condensation onto the sensor can be prevented by operating the heater.

In the humidity sensor which measures moisture content on the basis of change in the resistance of the moisture sensitive layer, the resistance of the moisture sensitive layer changes in accordance with the temperature of an atmosphere under detection; i.e., the resistance of the layer has temperature dependency. Therefore, as described in a fifth embodiment of the invention, the humidity sensor preferably comprises a temperature measurement resistor provided within the insulating substrate. Change in the resistance of the moisture sensitive layer with temperature is corrected by the temperature measurement resistor, and thus humidity can be detected at high accuracy independent of the temperature of the atmosphere. In addition to the ability of the moisture sensitive layer to measure the relative humidity of the atmosphere, the temperature measurement resistor can measure the temperature of the atmosphere. As a result, the absolute humidity of the atmosphere can also be measured.

As described in a sixth embodiment of the invention, preferably, the heater and the temperature measurement resistor provided in the insulating substrate are located directly below the moisture sensitive layer. When the heater is provided directly below the moisture sensitive layer, the entire moisture sensitive layer is easily heated in a substantially uniform manner, moisture and other impurities that have invaded the moisture sensitive layer can be removed efficiently, and the power consumption required for heating

the layer can be reduced to the greatest possible extent. Meanwhile, by providing the temperature measurement resistor directly below the moisture sensitive layer, the temperature of the atmosphere can be measured at a position which is substantially the same as the position at which the humidity  
5 is detected, without being affected by heat conduction of the insulating substrate. Therefore, accuracy in humidity detection can be further enhanced.

When the humidity sensor as described in the first embodiment has a specific structure as described in any of the second through sixth embodiments, even when the sensor is used in an atmosphere as defined in a  
10 seventh embodiment; i.e., an atmosphere containing a very small amount of oxygen and containing a reducing gas, the sensor maintains excellent detection performance over a long period of time. Therefore, the sensor is particularly useful for measuring the moisture content of a specific atmosphere in an exhaust pipe of an automobile or in a fuel cell. The expression "the amount of  
15 oxygen is very small" means an amount of oxygen as measured by a conventional apparatus at the detection limit or less; for example, an amount of about  $10^{-9}$  to  $10^{-20}$  atm. The expression "an atmosphere containing reducing gas" means an atmosphere containing a reducing gas (e.g., HC, CO, NO, H<sub>2</sub>) in a certain amount or more such that the reducing gas can bring about  
20 chemical equilibrium (e.g., CO = 3144 ppm, THC - total hydrocarbon (CH<sub>4</sub>, C<sub>3</sub>H<sub>6</sub>, C<sub>7</sub>H<sub>8</sub>, etc.) = 459 ppm, NO = 243ppm).



## BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1(a) is a schematic perspective view of a humidity sensor. Fig. 1(b) is a cross-sectional view of the humidity sensor taken along line A-A' of Fig. 1(a).

5        Fig. 2 is a graph showing a comparison in durability between the humidity sensor of the present invention and a conventional humidity sensor when these sensors are exposed to an atmosphere containing a large amount of oxygen and a very small amount of a reducing gas.

10       Fig. 3 is a graph showing a comparison in durability between the humidity sensor of the present invention and a conventional humidity sensor when these sensors are exposed to an atmosphere containing substantially no oxygen and containing a large amount of a reducing gas.

15       Fig. 4 is a graph showing a comparison in output impedance between the humidity sensor of the present invention and a conventional humidity sensor when relative humidity is changed.

Fig. 5 is a schematic representation showing an apparatus for evaluating detection characteristics of a humidity sensor by means of a shunting method.

### Description of Reference Numerals used in the Drawings:

- 20    1: humidity sensor  
     11: insulating substrate  
     111: heater  
     112: temperature measurement resistor

- 12: lower electrode
- 13: moisture sensitive layer
- 14: upper electrode
- 14a: a portion of upper electrode
- 5 14b: other portion of upper electrode
- 121, 141: output lead wires connected to electrodes
- 2: air cylinder
- 31: mass flow (wet)
- 32: mass flow (dry)
- 10 4: thermostatic chamber
- 51: first saturation bath
- 52: second saturation bath
- 6: evaluation container
- 7: temperature-humidity detection apparatus

## 15 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention will next be described in more detail by way of example. However, the present invention should be construed as being limited thereto.

### (1) Structure of humidity sensor

20 Fig. 1(a) is a perspective view showing an essential portion of a humidity sensor according to one embodiment of the present invention. Fig. 1(b) is a cross-sectional view of the humidity sensor taken along line A-A' in Fig. 1(a).

(i) Insulating substrate

An insulating substrate 11 is formed from  $\text{Al}_2\text{O}_3$ , and has a thickness of 1.6 mm, a width of 4 mm, and a length of 45 mm. A heater 111 which is formed from Pt and assumes the shape of a bent strip is provided in the  
5 insulating substrate located directly below a moisture sensitive layer at a position which is about 1/4 the thickness of the substrate distant from the lower surface of the substrate. A temperature measurement resistor 112 which is formed from Pt and assumes the shape of a bent strip is provided in the insulating substrate located directly below the moisture sensitive layer at a  
10 position which is about 1/4 the thickness of the substrate distant from the upper surface of the substrate.

(ii) Moisture sensitive layer, electrodes, etc.

A lower electrode 12 formed from Pt is joined to the upper surface at one longitudinal end of the insulating substrate. The lower electrode 12 is  
15 formed of a porous body having pores of 0.5-10  $\mu\text{m}$  and contains 12 wt.%  $\text{Al}_2\text{O}_3$ . The lower electrode 12 has a thickness of 30  $\mu\text{m}$ , a width of 2 mm, and a length of 2.5 mm. The lower surface of a moisture sensitive layer 13 formed from a moisture sensitive ceramic material containing  $\text{Al}_2\text{O}_3$  and predetermined amounts of  $\text{TiO}_2$  and  $\text{SnO}_2$  is joined to the entire surface of the  
20 lower electrode and a portion of the insulating substrate. The moisture sensitive layer 13 is formed of a porous body having pores of 0.05-0.2  $\mu\text{m}$ . The moisture sensitive layer 13 has a thickness of 400  $\mu\text{m}$ , a width of 2.5 mm,

and a length of 2.5 mm. An upper electrode 14 formed from Pt is joined to the upper surface of the moisture sensitive layer which is opposite the lower electrode; one side end surface of the moisture sensitive layer; and a portion of the upper surface of the insulating substrate. The thickness of the upper electrode 14 is 30  $\mu\text{m}$ . The upper electrode 14 is formed of a porous body having pores of 0.5-10  $\mu\text{m}$  and containing 12 wt.%  $\text{Al}_2\text{O}_3$ . A portion 14a of the upper electrode 14 provided on the upper surface of the moisture sensitive layer has a width of 2 mm and a length of 2 mm. A portion 14b of the upper electrode 14 provided on the upper surface of the insulating substrate has a width of 0.5 mm and a length of 2.5 mm.

Output lead wires 121 and 141 are connected to the lower electrode and the upper electrode, respectively, and the lead wires extend from the electrodes. The heater is connected to a power supply source, and the temperature measurement resistor is connected to a temperature detection circuit. The power supply source, the temperature detection circuit, and lead wires connected thereto are not illustrated for the sake of simplicity.

## (2) Production of humidity sensor

(i) Production of an insulation substrate having output lead wires thereon, and a heater and a temperature measurement resistor disposed within the substrate.

A slurry containing alumina powder was prepared, and alumina green sheets A, B, C and D (the entirety to serve as an insulating substrate 11 after firing) (thickness of each sheet: 450  $\mu\text{m}$ ) were formed from the slurry using a

doctor blade process. Thereafter, through screen printing, a Pt-containing paste for a heater was applied onto the upper surface of the alumina green sheet A, to thereby form a heater pattern (to serve as a heater 111 and a wire to be connected to a power supply source (not illustrated) after firing).

5        Through screen printing, a Pt-containing paste for a temperature measurement resistor was applied onto a first surface of the alumina green sheet C, to thereby form a temperature measurement resistor pattern (to serve as a temperature measurement resistor 112 and a wire to be connected to a temperature detection circuit (not illustrated) after firing). Furthermore,  
10        through screen printing, a Pt-containing paste for an output lead wire was applied onto a first surface of the alumina green sheet D, to thereby form output lead wire patterns (to serve as output lead wires 121 and 141 after firing).

Subsequently, the alumina green sheets A to D were stacked on one  
15        another, such that 1) a second surface of the alumina green sheet D (the output lead wire patterns having been formed on the first surface thereof) came into contact with the first surface of the alumina green sheet C on which the temperature measurement resistor pattern had been formed; 2) a second surface of the alumina green sheet C came into contact with a first surface of  
20        the alumina green sheet B, the sheet B serving as an insulating layer for further securing contact between the heater pattern and the temperature measurement resistor pattern; and 3) a second surface of the alumina green sheet B came into contact with a first surface of the alumina green sheet A on

which the heater pattern has been formed. The resultant product was pressed to thereby form a laminate. Thereafter, the resultant laminate was fired at 1,550°C for two hours, to thereby produce an insulating substrate in which a heater and a temperature measurement resistor were provided.

5        The dimensions of the green sheets were determined such that 10 insulating substrates could be produced. Heater patterns, temperature measurement resistor patterns, and output lead wire patterns were formed in a number corresponding to the number of the substrates. The green sheets were stacked as described above, and the resultant laminate was cut into green  
10        substrates. The resultant green substrates were fired to thereby produce 10 insulating substrates simultaneously.

(ii) Production of moisture sensitive layer

A powder mixture containing  $\text{Al}_2\text{O}_3$  powder and predetermined amounts of  $\text{TiO}_2$  powder and  $\text{SnO}_2$  powder was formed into a predetermined  
15        shape. Thereafter, the resultant product was fired at 1,200°C for two hours, to thereby produce a moisture sensitive layer having a thickness of 400  $\mu\text{m}$ , a width of 2.5 mm, and a length of 2.5 mm.

(iii) Production of humidity sensor

On a first surface of the moisture sensitive layer produced in (ii) above,  
20        a portion of an upper electrode pattern (to serve as a portion 14a of an upper electrode after firing) was printed using a platinum paste, and then dried, to thereby form a film having a thickness of 30  $\mu\text{m}$ , a width of 2 mm, and a length of 2 mm. Thereafter, a lower electrode pattern (to serve as a lower

electrode 12 after firing) was printed, using a platinum paste, on the upper surface of the insulating substrate produced in (i) above (the temperature measurement resistor is provided in the vicinity of the surface) at one longitudinal end of the substrate, and then dried, to thereby form a film having  
5 a thickness of 30  $\mu\text{m}$ , a width of 2 mm, and a length of 2.5 mm. Subsequently, the moisture sensitive layer was pressed onto the insulating substrate such that the lower surface of the moisture sensitive layer came into contact with the entire surface of the film and a portion of the upper surface of the substrate. Thereafter, in order to cause the moisture sensitive layer and the  
10 insulating substrate to adhere to each other sufficiently, and to secure conduction between an upper electrode 14 and an output lead wire 141, another portion of the upper electrode pattern (to serve as another portion 14b of the upper electrode after firing) was printed on one side end of the moisture sensitive layer and on a portion of the upper surface of the insulating substrate,  
15 such that the other portion was connected to the aforementioned portion of the upper electrode pattern, and then dried, to thereby form a film having a thickness of 30  $\mu\text{m}$ , a width of 0.5 mm, and a length of 2.5 mm.

Thereafter, the resultant laminate including the insulating substrate, the lower electrode pattern, the moisture sensitive layer, and the upper electrode  
20 pattern was fired at 1,200°C for 10 minutes, to thereby produce a humidity sensor.

### (3) Evaluation of durability of humidity sensor

(i) Evaluation in an atmosphere containing a large amount of oxygen and a very small amount of a reducing gas

The humidity sensor produced in (2), and a conventional humidity sensor in which lower and upper electrodes are formed from RuO<sub>2</sub> instead of Pt were exposed for 30 minutes, in an exhaust pipe of a diesel automobile, to exhaust gas containing a large amount of oxygen and a very small amount of reducing gas, and these sensors were evaluated in terms of time-course change in humidity detection characteristics. The temperature of the exhaust gas was changed from 100 to 700°C at intervals of 100°C, and the change in characteristics with respect to temperature was also evaluated. Fig. 2 shows the results when the sensors were evaluated by means of a shunting method at a relative humidity of 80%.

Composition of exhaust gas: O<sub>2</sub> (16%), CO<sub>2</sub> (3%), H<sub>2</sub>O (3%), other gasses (HC, NO, CO, etc.) (very small amounts, e.g., 500 ppm or less).

Evaluation method: After the humidity sensor was exposed to the exhaust gas of an actual automobile at the aforementioned temperatures, the detection characteristics of the sensor were measured by means of a shunting method (JIS Z 8806-1981), and the time-course change of the sensor with respect to the exhaust gas and the temperature thereof was evaluated.

Evaluation conditions: measurement temperature (20°C), evaluation gas (air), relative humidity (40%, 60%, 80%, or 90%).

In this embodiment, as shown in Fig. 5, evaluation gas is supplied through each line from air cylinder 2. Adjusting the volume of the evaluation



gas in mass flow (dry) 32 and in mass flow (wet) 31 to predetermined values, evaluation gas is supplied through thermostatic chamber 4 into evaluation container 6 in which the resistance changing characteristics of the humidity sensor 1 with respect to a change in humidity is measured. Additionally the  
5 predetermined values of the evaluation gas supplied to the evaluation container are confirmed by a temperature-humidity detection apparatus 7.

The thermostatic chamber 4 is adjusted to 20 °C and the total flow rate of the mass flow 31, 32 is adjusted to 5 liters/min. Further, the first saturation bath 51 and the second saturation bath 52 are each provided in a wet line  
10 between the mass flow wet 31 and the evaluation container 6 so as to saturate the evaluation gas.

As shown in Fig. 2, the humidity sensor produced in (2) in which the upper and lower electrodes are formed from Pt exhibited no significant difference from the conventional humidity sensor having a structure similar to  
15 that of the above humidity sensor except that the upper and lower electrodes are formed from RuO<sub>2</sub>, in that the detection characteristics do not vary regardless of exposure to the exhaust gas or variation in the temperature of the exhaust gas. Therefore, when being exposed to an atmosphere containing a large amount of oxygen and a very small amount of reducing gas, RuO<sub>2</sub> as  
20 well as Pt effectively functions as an electrode of the humidity sensor.

(ii) Evaluation in an atmosphere containing substantially no oxygen and containing a large amount of a reducing gas

The humidity sensor produced in (2) and a conventional humidity sensor in which lower and upper electrodes are formed from RuO<sub>2</sub> instead of Pt were exposed for 30 minutes, in an exhaust pipe of a gasoline automobile engine (air-fuel ratio was regulated to 14.0), to exhaust gas containing substantially no oxygen and containing a large amount of a reducing gas, and these sensors were evaluated in terms of the time-course change in humidity detection characteristics. The temperature of the exhaust gas was changed from 200 to 700°C at intervals of 100°C, and the change in characteristics with respect to temperature was also evaluated. Fig. 3 shows the results when the sensors were evaluated by means of a shunting method at relative humidities of 60% and 80%.

Composition of exhaust gas: O<sub>2</sub> (substantially not present), CO<sub>2</sub> (10%), H<sub>2</sub>O (10%), other gasses (HC, NO, CO, etc.) (very small amounts, e.g., 500 ppm or less).

Evaluation method and evaluation conditions were similar to those in the case of (i).

As shown in Fig. 3, in the case of the humidity sensor produced in (2) in which the upper and lower electrodes are formed from Pt, detection characteristics do not vary, regardless of exposure to the exhaust gas or variation in the temperature of the exhaust gas. Therefore, even when the humidity sensor is exposed to an atmosphere which undergoes a drastic change in temperature, or to an atmosphere containing a very small amount of oxygen and a large amount of a reducing gas, the humidity sensor does not

lose its function as a humidity sensor and exhibits excellent durability. In contrast, in the case of the conventional humidity sensor in which the upper and lower electrodes are formed from RuO<sub>2</sub>, the resistance substantially increases when the temperature of the exhaust gas is approximately 400-  
5 500°C. As shown in Fig. 4, when the temperature of the exhaust gas is 600°C or higher, the impedance of the conventional humidity sensor becomes approximately 1.00E+08 Ω, regardless of the relative humidity; i.e., the sensor does not function as a humidity sensor.

### EFFECTS OF THE INVENTION

10 The first embodiment of the invention provides a humidity sensor of high accuracy exhibiting excellent durability, in which the strength of adhesion between an insulating substrate and a moisture sensitive layer is enhanced. Particularly, when the humidity sensor has a specific structure as described in the second through sixth embodiments, even if the sensor is used  
15 in a specific atmosphere as described in the seventh embodiment, the sensor exhibits high accuracy and excellent durability.

It should further be apparent to those skilled in the art that various changes in form and detail of the invention as shown and described above may be made. It is intended that such changes be included within the spirit and  
20 scope of the claims appended hereto.

This application is based on Japanese Patent Application No. 2000-309169 filed October 10, 2000, the disclosure of which is incorporated herein by reference in its entirety.